DETERMINATION OF THE FREE VOLUME AND THE ENTROPY BY A MONTE CARLO METHOD

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ARSTRACT

The configurational integral can in principle, though not in practice, be determined from the ratio of accepted to rejected moves $(\langle a_N(v)\rangle)$ in the Monte Carlo method of Metropolis et al., if the moves consist of simultaneous random displacements of N particles uniformly distributed over the sample volume v. In the usual Monte Carlo process only one particle at a time is displaced within a small volume. If this volume is suitably chosen (v_D) , the acceptance ratio $(\langle a_1(v_D)\rangle)$ determines the mean free volume per particle $(v_f = v_D \langle a_1(v_D)\rangle)$. Evidence is presented supporting the approximate validity of the relationship $\langle a_N(v)\rangle = \langle a_1(v_D)\rangle^N$ which permits the evaluation of the configurational integral. The entropies calculated in this way for a system of 108 Lennard–Jones particles with parameters corresponding to argon, are in good agreement with the experimental values for solid and liquid argon. The results indicate that the full amount of the communal entropy appears on fusion.

In the well-known Monte Carlo (MC) method of Metropolis et al. certain many-dimensional integrals containing the Boltzmann factor as weighting function are evaluated by means of the following procedure: configurations of a system of N particles are generated by small random displacements of single particles; if \mathbf{r}_{α}^{N} is the configuration after α moves and the next trial move leads to \mathbf{r}_{α}^{N} , then this move is rejected (by setting $\mathbf{r}_{\alpha+1}^{N} = \mathbf{r}_{\alpha}^{N}$) if and only if the difference between the potential energies $\Phi(\mathbf{r}_{\alpha}^{N}) - \Phi(\mathbf{r}_{\alpha}^{N}) = \Delta_{\alpha}\Phi > 0$ and $\exp(-\Delta_{\alpha}\Phi/kT) < \eta$, η being a number chosen at random between 0 and 1; otherwise the move is accepted (by setting $\mathbf{r}_{\alpha+1}^{N} = \mathbf{r}_{\alpha}^{N}$).

If in this process configurations were generated by simultaneous displacements of all N particles to random positions uniformly distributed over the sample volume v, the configurational integral could in principle be evaluated from the mean acceptance ratio for the trial moves

$$\frac{\int_{0}^{L} \dots \int_{0}^{L} \exp\left[-\left\{\Phi(\mathbf{r}^{N}) - \Phi_{\min}\right\}/kT\right] \, d\mathbf{r}^{N}}{\int_{0}^{L} \dots \int_{0}^{L} d\mathbf{r}^{N}} = \frac{Q'(NvT) \exp\left(\Phi_{\min}/kT\right)}{v^{N}}$$

$$= \lim_{M \to \infty} \sum_{\alpha=1}^{M} \frac{\exp\left[-\left\{\Phi(\mathbf{r}^{N}_{\alpha}) - \Phi_{\min}\right\}/kT\right]}{M} = \frac{\text{no. of accepted moves}}{\text{no. of attempted moves}}$$

$$= \langle a_{N}(v) \rangle \tag{1}$$

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Table 1. Comparison of the statistics of consecutive acceptances (runs) of MC moves with the corresponding statistics for independent events of equal probability, calculated with the formula² $f(M) = M(1-p) p^a/(1-p^a)$, with $p = \langle a_1(v_d) \rangle$, $v_d = (4\pi/3) R_d^3$

	T =	50.0	V = 2	24-24	N = 26	= 108
а	2	8		20	26	32
$f_{ m obs.}$	51375	7922	2619	1032	403	175
	51375 51376	7900	2619 2619	1010	410	170
$f_{ m cate.}$	31370	7300			710	170
	T =	97·0	V = 2	28-48	N =	= 108
а	2	11	20	29 668	38	47
$f_{ m obs.}$	54540	5881	1776	668	241	103
feale.	54540		1808	654	250	97
Jealc.						
		97:0	V = 2	28-48	N =	
а	2	11		29	38	47
$f_{ m obs.}$	69528	6461	1632	488	129	38
$f_{ m calc.}$	69482	6439	1626	473	143	44
	T =	97:0	V = 2	28.48	N	= 108
a	2	4	6	8	10	12
			2898	943	215	0.5
$f_{\rm obs.}$	36428 36371	9089	2840	943	315	104
$f_{ m calc.}$	363/1	9137	2840	931	311	104
	T =	97.0	V = 1	28·48	<i>N</i> =	= 108
a	2	4	6	8	10	12
$f_{ m obs.}$	32407	7427	2068	607	175	53
$f_{\rm calc}$	32517	7379	2031	585	171	50
J care.					3.7	100
	T =		V = 2	28·48 8	N =	
a	2	4	6	_	10	12
$f_{ m obs.}$	28700			333	91	27
$f_{ m calc.}$	28544	5/11	1360	336	84	21
	T =	97.0	V = 3	28-48	N =	= 108
a	2	4	6	8	10	12
$f_{ m obs.}$	25043	4419	938	207	36	13
$f_{\rm calc.}$	25043 25165	4419 4446	938 919	196	42	9
Jeale.						
	T =	97.0	V = 1		N =	= 108
a	1	2	3	4		
$f_{ m obs.}$	2842	57	0	0		
$f_{ m cale,}$	2842	60	1	0		
	T =	97:0	V = 1	28-48	N =	= 256
а	1	2	3	4	• •	200
	6402		ő	ò		
$f_{\text{obs.}}$		134	3	0		
$f_{ m calc.}$			3	Ū		
	T =	298.2	V =	69-98		= 108
a	2	24		68	90	112
$f_{ m obs.}$	60098	3117	980 948	342	143	62
$f_{ m calc.}$	60098 60082	3109	948	355	143 142	58
	T =		V =	60.08	<i>N</i> =	
a	1 =	298.2	V = 3	4	5 IN =	= 108
		3 4 60	567	94	17	5
$f_{ m obs.}$	24269 24269	3460 3467	564	94 94	16	3
$f_{ m calc.}$	24209	3407	JU 4	74	10	

T is temperature in ${}^{\circ}K$.

 R_d is range of displacements in Å.

V is volume in cm³ mole⁻¹. N is number of particles.

M is number of attempted displacements.

a is number of displacements accepted consecutively (length of run). $f_{\rm obs.}$ and $f_{\rm calc}$ are the observed and calculated frequences of the number of displacements accepted consecutively.

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	M = 12800		$R_d = 0$	065	
38	44	50	56	62	68
80	32	14	7	3	0
71	30	12	5	2	1
	M = 127600		$R_d = 0$	069	
56	65	74	83	92	101
47	24	9	6	2	1
38	15	6	2	1	0
	M = 169600		$R_d = 0$	-086	
56	65	74	83	92	
12	4	2	1	0	
13	4	1	0	0	
	M = 170800		$R_d = 0$	-310	
14	M = 170800	18	$R_d = 0$	22	
29	15	5	1	0	
35	12	4	1	ő	
	M = 170800		$R_d = 0$.211	
14	M = 170800		$\mathbf{K}_d = 0$	7344	
16	3				
15	4				
	M 171200		D 0	270	
14	M = 171200	18	$R_d = 0$.319	
7	3	3	0		
5	1	0	0		
		V			
	M = 171600	40	$R_d = 0$	413	
14	16	18	20		
5 2	3	1	0		
2	U	U			
	M=132800		$R_d = 2$	÷07	
	1.5 200000			.05	
	M=299008		$R_d=2$.07	
	M = 127600		$R_d = 0$)·116	
134	156	178	200	222	244
31	11	8	5	2	1
24	10	4	2	1	0
	M = 145600		$R_d = I$	$R_D = 11.62$	
7	8	9	u -	.	
1	1	0			
0	0	0			

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 $(\Phi_{\min}]$ is the lowest potential energy attained, and the angular bracket indicates an ensemble average; $v = L^3$).

This method is impracticable because the acceptance ratio $\langle a_N(v) \rangle$ is too small and the numerical labour too great. Both difficulties are overcome in the usual process by the displacement of one particle at a time within a small volume $v_d \langle v \rangle$, centred on the current position of the particle. The mean acceptance ratio, $\langle a_1(v_d) \rangle$, has no physical significance here. When the range of attempted displacements is increased, the product $v_d \langle a_1(v_d) \rangle$ increases up to a limiting value v_d^* such that for $v_D \geqslant v_d^*$ the probability of acceptance of moves ending outside v_D it is virtually zero. For solids and liquids not too near the critical point, $v_D < v/N$; for fluids of lower density even large displacements are accepted, i.e. $v_D = v$. The acceptance ratio $\langle a_1(v_D) \rangle$ is the MC estimate of the integral

$$\langle \int \exp(-(\Phi^{1}(\mathbf{r}_{1}) - \Phi^{1}_{\min})/kT) \, d\mathbf{r}_{1} \rangle_{N-1}/v_{D}$$
 (2)

where $\Phi^1(\mathbf{r}_1)$ and Φ^1_{\min} are the energy of particle 1 and its minimum value within v_D , and the subscript N-1 indicates an average over all configurations of particles 2 to N. The numerator of expression 2 can be interpreted as defining the free volume, v_C .

The evaluation of the configurational integral is based on the proposition that, to a sufficient approximation,

$$\langle a_N(v) \rangle = \langle a_1(v) \rangle^N$$
 (3)

First, it will be noted that the acceptance ratio for displacements over the whole volume v can be determined from

$$v_{\mathbf{D}}\langle a_1(v_{\mathbf{D}})\rangle = v\langle a_1(v)\rangle \tag{4}$$

(for dense systems $\langle a_1(v) \rangle$ is too small to be obtained directly.) Secondly, since the MC evaluation of a many-dimensional integral can be effected either by sampling the different dimensions simultaneously or consecutively (in cycles)

$$\langle a_N(v) \rangle = \langle a_1(v)^N \rangle$$
 (5)

i.e. the mean probability of acceptance of a simultaneous displacement of N particles equals the joint probability of acceptance of N successive moves of one particle at a time. Thirdly, numerical experiments indicate that

$$\langle a_1(v)^N \rangle = \langle a_1(v) \rangle^N$$
 (6)

The statistics of runs of acceptances in the MC process have been compared with the known statistics of runs of independent events². The results are summarized in *Table 1*. To obtain runs of length N = 108, it is necessary to reduce the range of displacements, R_d , drastically. Alternatively, when R_d equals the radius of the spherical volume v_D , only short runs are obtained. Under both these conditions the observed statistics agree closely with the statistics of independent events. Although this evidence for the validity of equation 6 is not entirely conclusive, it does indicate that the two sides of 6

Table 2. Data for the calculation of entropies and comparison with the entropy of argon

Š.	A .	L	M .	$\langle a_1(v_D) \rangle$	$N_0 v_f$	R_D	(4) - 6min.	SMC	Sargon
	cm.mol	4	eoI		cm-mol .	A	A B	A B n	. 101
1. a, f	24·24 (c)	50-0	566	0.0240	0.092	1.18	0.166 0.535	22.6 24.6	23·3 d
2. b, f	24·24 (c)	86.3	176	0.00885	0.167	1.67	0.124 —		1
3. b, f	24·51 (c)	86.3	566	0.00891	0.171	1.97	0.147 0.757		38.8 d
4. b, g	28-48 (1)	97.0	398	0.0210	0.467	2.07	0.204 0.613		55.9 e
ပ်	28.48 (1)	97.0	298	0.0214	0.476	2.07	0.180 0.631		55.9 e
6. b, g	29-69 (1)	97.0	266	0.0265	0.615	2.10	0.216 —		58.4 e
ď,	29-69 (1)	97.0	133	0.0281	0.652	2.10	0.229 0.595		58.4 e
Ą	28-48 (1)	108.0	266	0.0224	0.499	2.07	0.245 0.570		58·5 e
ď,	28-48 (1)	136.0	566	0.0232	0.516	2.27	0.196 0.545		63·3 e
ď,	38-01 (1)	1360	180	0.0804	3.04	2.46	0.180 0.475		74·6 e
ď,	(g) 86-69	173.2	146	0.121	8-47	11.62	0.245 —		91·0 d
12. b, h	(g) 86·69	298.2	297	0.1634	12.35	11.62	0.138 0.306		100·6 d

a: N=108, LJ parameters g/k=117, $z_0=3405$ Å (ref. 3). b: N=108 LJ parameters g/k=1198, $\sigma=3405$ Å (ref. 7). c: N=256, LJ parameters g/k=1198, $\sigma=3405$ Å (ref. 7). d: interpolated from data in ref. 8. e: interpolated from data in ref. 9. f: $C_1=1$ g: $C=N^N/N$ 1 h: C=1/N1. Then the description of the control of the con

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differ by less than an order of magnitude. A small error would have little effect on the entropy: since

$$S/Nk = (1/N) \log (v^N \langle a_1(v)^N \rangle) + \text{ other terms,}$$

a discrepancy by a factor ten between the two sides of 6 would (with N=108) lead to an error of less than three per cent in the configurational entropy. The configurational partition function can therefore be written in the form

$$Q = C \exp\left(-\Phi_{\min}/kT\right) (v\langle a_1(v)\rangle)^N = C \exp\left(-\Phi_{\min}/kT\right) v_f^N \tag{7}$$

The value of C depends on the nature of the system: for localized particles (in solids), C=1; for dense fluids, when $v_D < v/N$, $C=N^N/N!$; for fluids of lower density, when $v_D=v$, C=1/N!. There is a (not very extensive) region below the critical temperature where $v/N < v_D < v$, when the present method is not applicable.

Entropies have been calculated with the formula

$$S/Nk = (\langle \Phi \rangle - \Phi_{\min})/NkT + 1.5 \{ 1 + \log(2\pi mkT/h^2) \} + (1/N)\log C + \log v_f$$
 (9)

for a model consisting of 108 (or 256) Lennard-Jones (12-6) particles with parameters corresponding to argon. As a first approximation Φ_{\min} was equated to the lowest total potential energy attained in the MC experiment (method A). Table 2 shows that this leads to entropies which are consistently by about eight per cent lower than the experimental values. This procedure is also unsatisfactory because $(\langle \Phi \rangle - \Phi_{\min})/NkT$ estimated in this manner varies as $N^{-1/2}$ instead of being an intensive quantity. This objection does not hold if Φ_{\min} is set equal to $(N/2) \langle \Phi^1_{\min} \rangle$ where $\langle \Phi^1_{\min} \rangle$ is the mean value of the minimum of the potential energy of a particle in the field of the other particles. This step may be further justified as follows. Equation 2 can be written in the form

$$\langle a_1(v) \rangle = \langle \int F_1(\mathbf{r}^N) \, d\mathbf{r}_1 \rangle_{N-1} / v$$

$$\equiv \int \dots \int (F_N/F_1) \, d\mathbf{r}_2 \dots d\mathbf{r}_N \int F_1 \, d\mathbf{r}_1 / \int \dots \int (F_N/F_1) \, d\mathbf{r}_2 \dots d\mathbf{r}_N \int d\mathbf{r}_1$$

where $F_N = \exp(-(\Phi(\mathbf{r}^N) - \Phi_{\min})/kT)$. If equations 5 and 6 are to be valid, one must equate F_1 to

$$\exp(-(\Phi^{1}(\mathbf{r}^{N}) - \Phi_{\min}^{1}(\mathbf{r}_{2},..,\mathbf{r}_{N}))/2kT)$$

and

$$\Phi_{\min}$$
 to $N\langle\Phi_{\min}^1\rangle/2$,

where

$$\Phi^{1}(\mathbf{r}^{N}) = \sum_{j=2}^{N} \varphi(|\mathbf{r}_{j} - \mathbf{r}_{1}|)$$

and

$$\Phi_{\min}^{1}(\mathbf{r}_{2},\ldots,\mathbf{r}_{N}) = \sum_{j=2}^{N} \varphi(|\mathbf{r}_{i}-\mathbf{r}_{1(\min,j)}(\mathbf{r}_{2},\ldots,\mathbf{r}_{N})|).$$

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 $\langle \Phi_{\min}^1 \rangle$ is determined from separate MC data. The values so obtained are in satisfactory agreement with the experimental entropies for solid and liquid argon (*Table 2*, method B). The persistent discrepancy for the gaseous V, T point is almost certainly due to the difficulty of determining $\langle \Phi_{\min}^1 \rangle$ in this case.

In spite of this uncertainty, which calls for further investigation, the present methods has some advantages compared with the MC method employed in the impressive work of Hansen and Verlet⁴. The statistical convergence of the acceptance ratio is excellent and the statistical error in the entropies after 2 to 3×10^5 moves is of the order of one per cent. This compares very favourably with the accuracy of the MC estimate of pressure which is required in methods based on the integration of p dv along isotherms⁴. Moreover, whereas the evaluation by the latter method of the free energy and entropy at one V,T point requires MC pressure data for $\simeq 12 \ V,T$ points, the proposed method requires data for one V, T point only. A similar saving of computational labour applies to MC calculations of the free energy of mixtures: these have been evaluated by integration with respect to continuously varying parameters along an isotherm⁵. The most promising field of application of the present method is perhaps the calculation of the free volume and the entropy of different molecular and ionic species in mixtures.

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